

New Criteria for the Eduction of Three-Dimensional Turbulent Structures

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Introduction

Existing criteria for turbulent structure eduction

multiple definitions of a vortex \Rightarrow multiple criteria

- spiraling (locally linearized) trajectories
Chong, Perry & Cantwell '90: Δ
Chakraborty, Balachandar & Adrian '05
- balance between shear and rotation
Hunt, Wray & Moin '88: Q
- approximated local minima of pressure
Jeong & Hussain '95: λ_2
- combination of definitions
Kida & Miura '98
Horiuti '01

Introduction

Geometrical interpretation for 2D flows

- incompressible flows: $\Delta, Q, \lambda_2 \rightarrow$ (Okubo–) Weiss '81, '91 criterion
- Weiss criterion recasted using streamfunction ψ

$$\frac{\partial^2 \psi}{\partial x^2} \frac{\partial^2 \psi}{\partial x^2} - \left(\frac{\partial^2 \psi}{\partial x \partial y} \right)^2 > 0 \quad \Leftrightarrow \quad \text{convex streamlines}$$

- alternative definition: region of convex isovorticity lines

$$\frac{\partial^2 \omega}{\partial x^2} \frac{\partial^2 \omega}{\partial x^2} - \left(\frac{\partial^2 \omega}{\partial x \partial y} \right)^2 > 0 \quad \text{Herbert, Larchevêque \& Staquet '96}$$

- advantages:

- educe thinner structures than Weiss criterion
- well correlated with dynamically active regions of the flow

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Mathematical definitions

Curvature in 3D space (1)

- local analysis of isosurfaces of the vorticity norm $\omega = \|\underline{\omega}\|$
- Taylor expansion with M and M_0 on the same isosurface

$$\frac{1}{2} \underline{MM_0}^T \underline{\underline{H}}(\omega) \Big|_{M_0} \underline{MM_0} + \underline{\nabla}(\omega) \Big|_{M_0} \cdot \underline{MM_0} = O\left(\|\underline{MM_0}\|^3\right)$$

- Hessian matrix and gradient vector
 - $\underline{\underline{H}}(\omega)$ symmetric \rightarrow diagonalizable:

$$\underline{\underline{H}}(\omega) \Big|_{(\underline{e}_1, \underline{e}_2, \underline{e}_3)} = \begin{pmatrix} \lambda_1 & & \\ & \lambda_2 & \\ & & \lambda_3 \end{pmatrix}$$

- gradient in the frame $(\underline{e}_1, \underline{e}_2, \underline{e}_3)$:

$$\underline{\nabla}(\omega) \Big|_{M_0} = a_1 \underline{e}_1 + a_2 \underline{e}_2 + a_3 \underline{e}_3$$

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Mathematical definitions

Curvature in 3D space (2)

- S locally described in the frame $(M_0, \underline{e}_1, \underline{e}_2, \underline{e}_3)$ by:

$$\lambda_1 \left(X_1 + \frac{a_1}{\lambda_1} \right)^2 + \lambda_2 \left(X_2 + \frac{a_2}{\lambda_2} \right)^2 + \lambda_3 \left(X_3 + \frac{a_3}{\lambda_3} \right)^2 = \frac{a_1^2}{\lambda_1} + \frac{a_2^2}{\lambda_2} + \frac{a_3^2}{\lambda_3}$$

Quadric with axis $(\underline{e}_1, \underline{e}_2, \underline{e}_3)$ centered on $C : \left(\frac{-a_1}{\lambda_1}, \frac{-a_2}{\lambda_2}, \frac{-a_3}{\lambda_3} \right)$

- exact mean curvature \mathcal{H} at location M_0

$$\mathcal{H} = \frac{\underline{\nabla}(\omega)_{|M_0}^T \underline{\underline{H}}(\omega)_{|M_0} \underline{\nabla}(\omega)_{|M_0} - \text{Tr}(\underline{\underline{H}}(\omega)_{|M_0}) \left\| \underline{\nabla}(\omega)_{|M_0} \right\|^2}{2 \left\| \underline{\nabla}(\omega)_{|M_0} \right\|^3}$$

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Mathematical definitions

Classification

- using the eigenvalues

- 3 negative eigenvalues: $\begin{cases} \text{ellipsoid} \\ \text{maxima of } \omega \end{cases}$
- 2 negative eigenvalues: $\begin{cases} \text{hyperboloid} \\ \text{saddle point maxima of } \omega \end{cases}$

- using the main invariants

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- using the main invariants

$$\begin{cases} I_1 = \text{Tr}\left[\underline{\underline{H}}(\omega)\right] & = \lambda_1 + \lambda_2 + \lambda_3 \\ I_2 = \frac{1}{2} \left\{ \text{Tr}\left[\underline{\underline{H}}(\omega)\right]^2 - \text{Tr}\left[\underline{\underline{H}}(\omega)^2\right] \right\} & = \lambda_1 \lambda_2 + \lambda_1 \lambda_3 + \lambda_2 \lambda_3 \\ I_3 = \text{Det}\left[\underline{\underline{H}}(\omega)\right] & = \lambda_1 \lambda_2 \lambda_3 \end{cases}$$

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- $\left. \begin{array}{l} I_1 < 0 \\ I_2 > 0 \\ I_3 < 0 \end{array} \right\} : \left\{ \begin{array}{l} \text{ellipsoid} \\ \text{maxima of } \omega \end{array} \right.$
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 $I_3 < 0$ }: $\left\{ \begin{array}{l} \text{ellipsoid} \\ \text{maxima of } \omega \end{array} \right.$ → pancake (H_ω^p)
- $I_1 < 0$
 $I_3 > 0$ }: $\left\{ \begin{array}{l} \text{hyperboloid} \\ \text{saddle point maxima of } \omega \end{array} \right.$ → tube / layer

Mathematical definitions

Refined classification

- separating tube and layer / sheet

- slenderness governed by I_2 : $I_2 > 0 \Leftrightarrow \lambda_3 < \frac{\lambda_1\lambda_2}{|\lambda_1 + \lambda_2|}$

$I_2 > 0 \rightarrow$ tube (H_ω^t)

$I_2 \leq 0 \rightarrow$ layer / sheet

- separating rotational layer and sheet

- difficult to achieve using invariants

physical consideration

$Q > 0 \rightarrow$ rotational layer ($H_\omega^{rl_Q}$)

$Q \leq 0 \rightarrow$ sheet ($H_\omega^{s_Q}$)

geometrical consideration

$\mathcal{H} > 0 \rightarrow$ rotational layer ($H_\omega^{rl_H}$)

$\mathcal{H} \leq 0 \rightarrow$ sheet ($H_\omega^{s_H}$)

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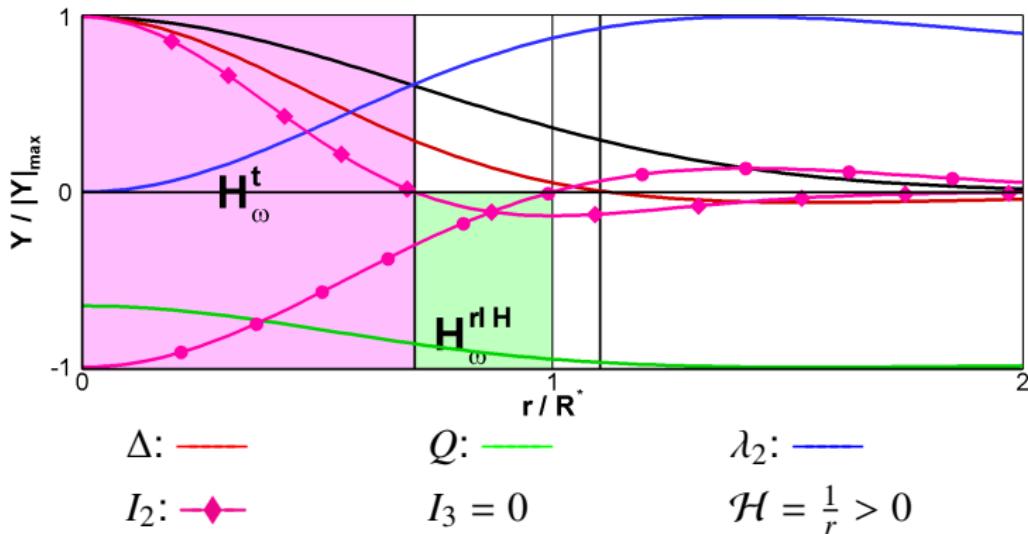
$\mathcal{H} > 0 \rightarrow \text{rotational layer } (H_\omega^{rl\mathcal{H}})$

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Test cases

Burgers' vortex tube

$\text{Re}=1$



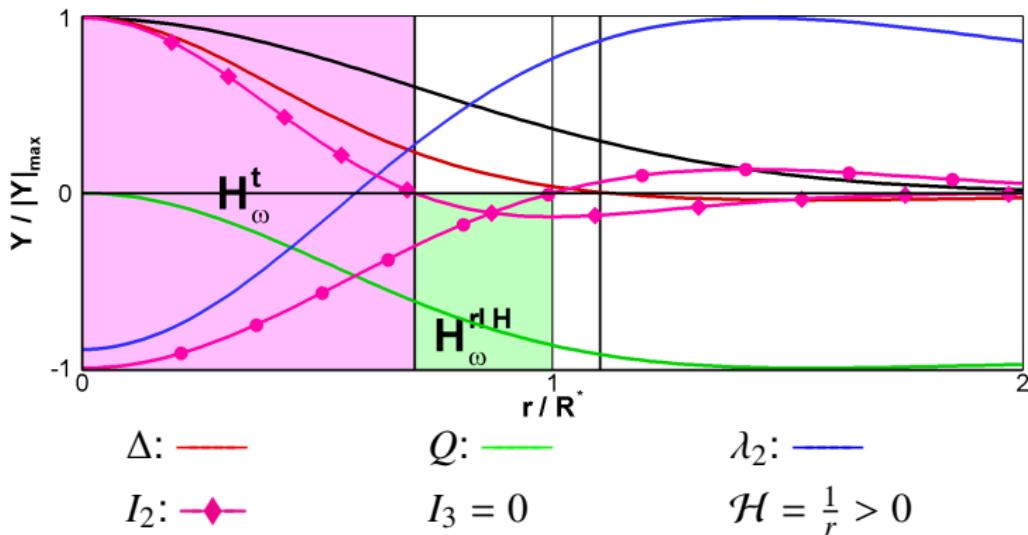
- H_ω criteria relying on \mathcal{H} : insensitive to transverse shear
- $I_1 \leq 0$ corresponds to the “classical” definition of the vortex core:

$$r \leq R^* = 2 \sqrt{\frac{\nu}{\alpha}}$$

Test cases

Burgers' vortex tube

$$Re = \sqrt{3}$$



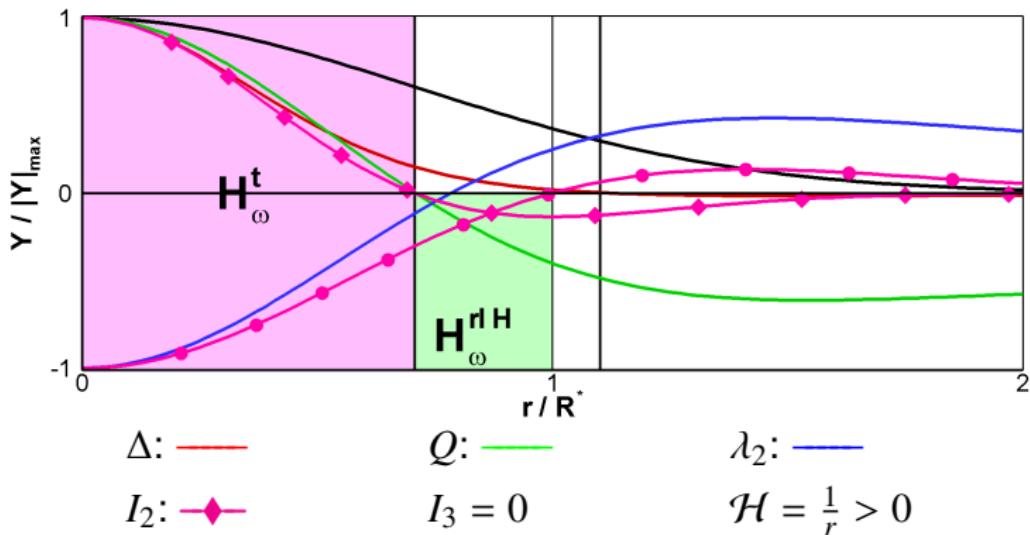
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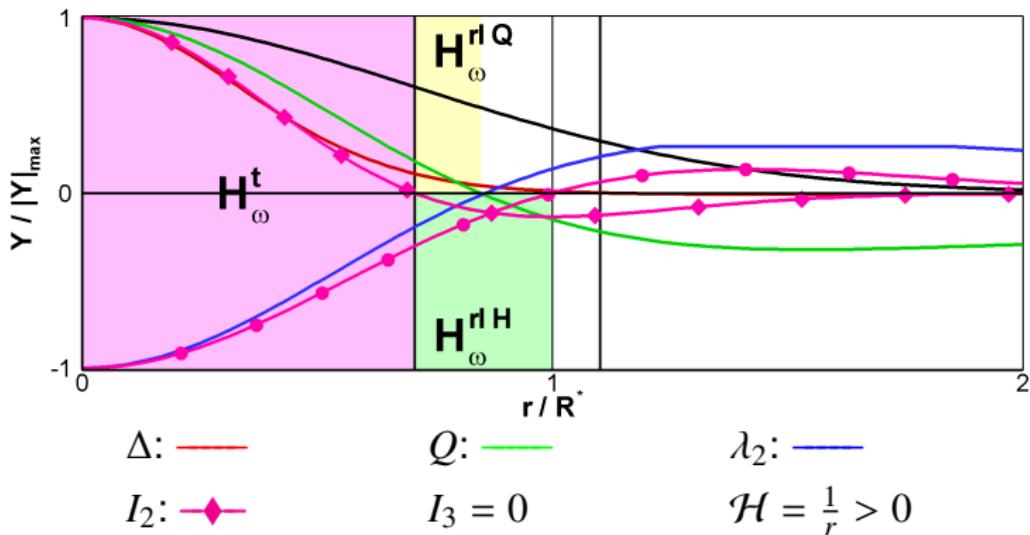
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Test cases

Burgers' vortex tube

Re=4



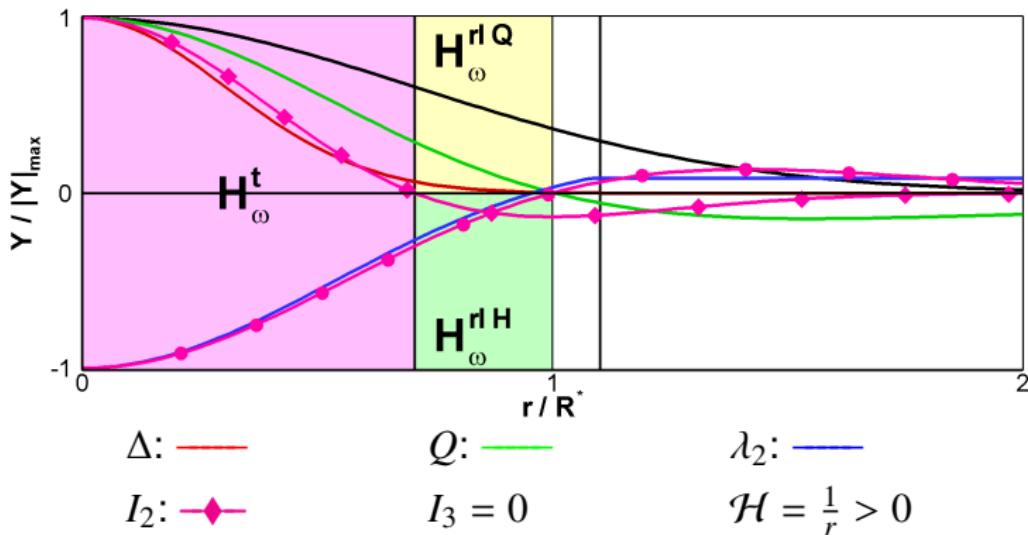
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Test cases

Burgers' vortex tube

$Re = 4\sqrt{3}$



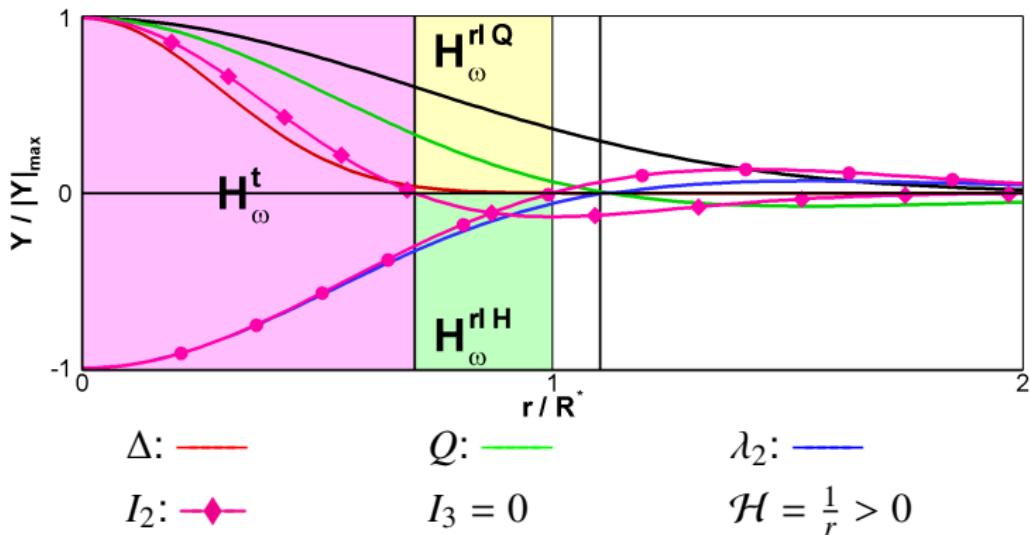
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Test cases

Burgers' vortex tube

Re=100



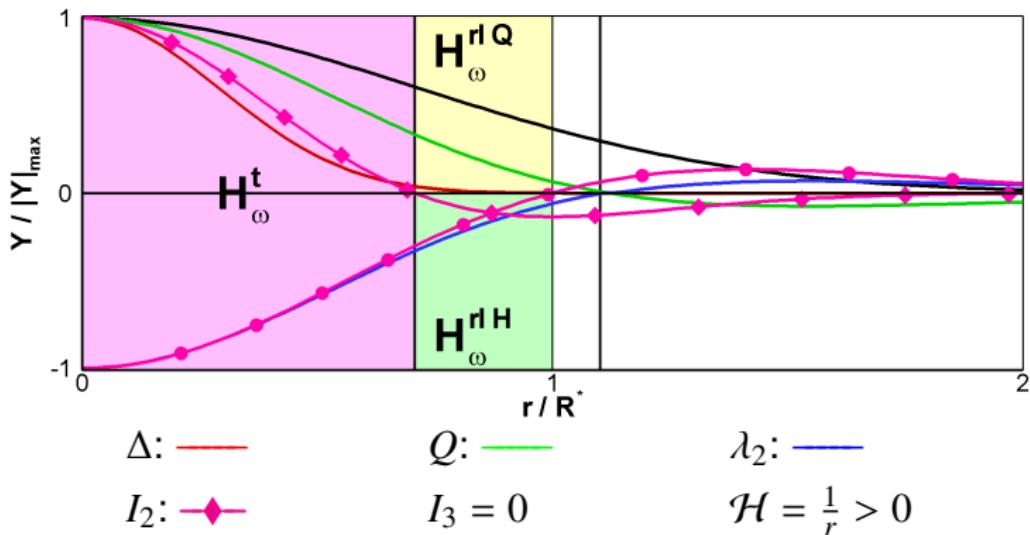
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Test cases

Burgers' vortex tube

Re=100



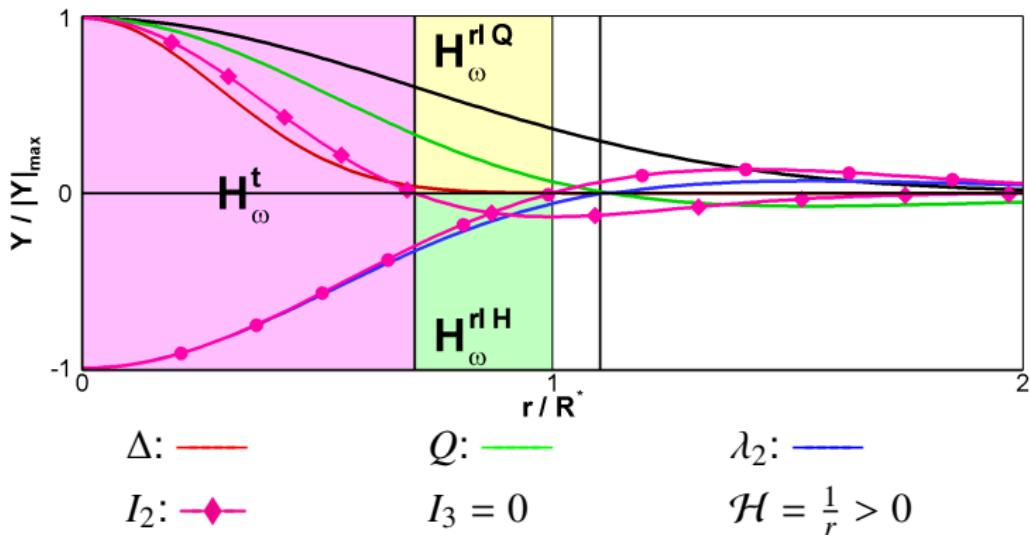
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Test cases

Burgers' vortex layer

$$\begin{cases} \underline{u} = U(x_2) \underline{i}_1 - \alpha x_2 \underline{i}_2 + \alpha x_3 \underline{i}_3 \\ \omega = -U'(x_2) = \frac{\gamma}{\sqrt{2\pi}} \sqrt{\frac{\alpha}{\nu}} \exp\left(\frac{-\alpha x_2^2}{2\nu}\right) \end{cases}$$

- $\Delta = \alpha^6 > 0$
- $Q = -\alpha^2 < 0$
- $\lambda_2 = \frac{1}{2} \left[\alpha^2 + \sqrt{\alpha^2 (1 + U'(x_2)^2)} \right] > 0$

Test cases

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The three criteria exclude the whole layer

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- $I_1 = -\frac{\gamma}{\sqrt{2\pi}} \left(\frac{\alpha}{\nu}\right)^{\frac{3}{2}} \exp\left(\frac{-\alpha x_2^2}{2\nu}\right) \left(1 - \frac{\alpha}{\nu} x_2^2\right)$ $I_2 = I_3 = \mathcal{H} = 0$

Test cases

Burgers' vortex layer

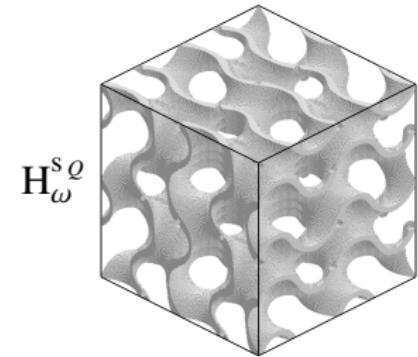
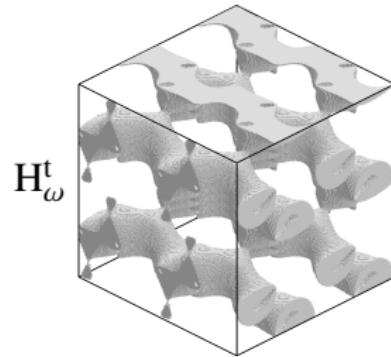
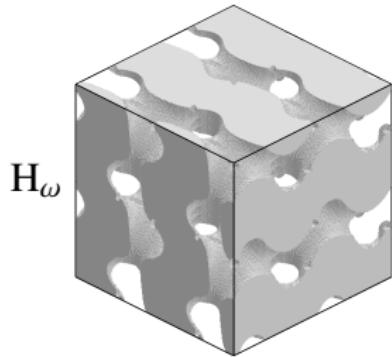
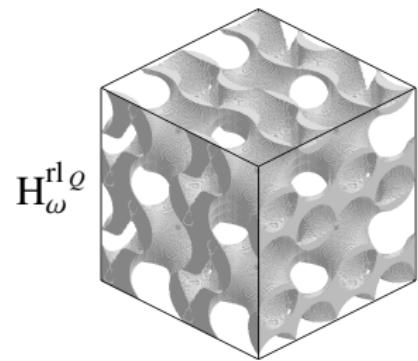
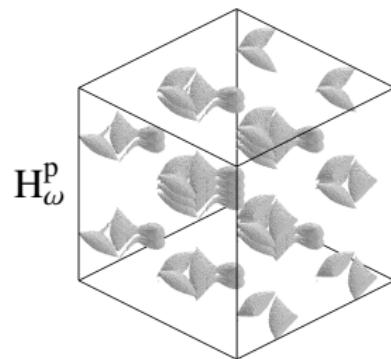
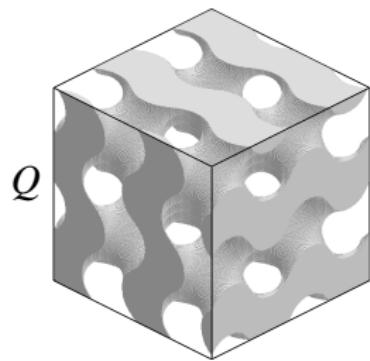
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- $I_1 < 0 \quad \Leftrightarrow \quad |x_2| < \delta \equiv \sqrt{\frac{\nu}{\alpha}}$

Both $H_{\omega}^{s_Q}$ and $H_{\omega}^{s_H}$ criteria **educe the whole layer**

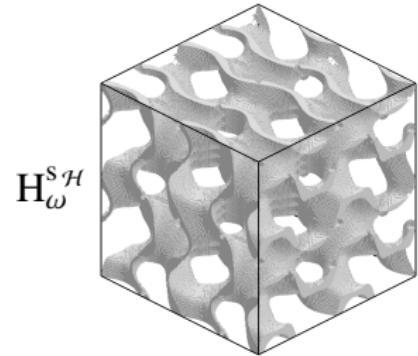
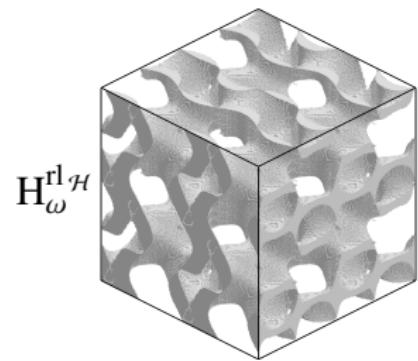
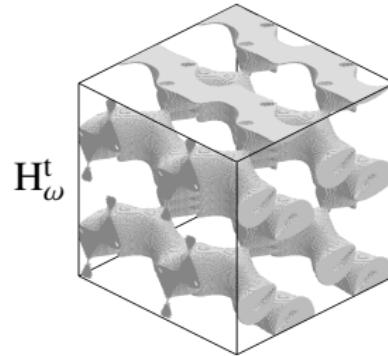
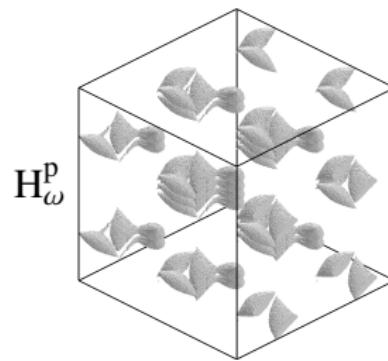
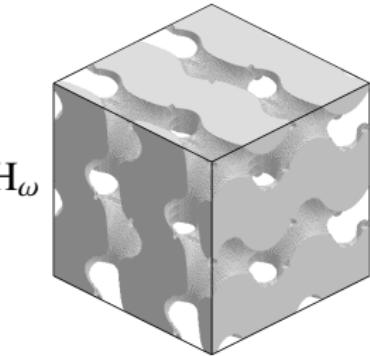
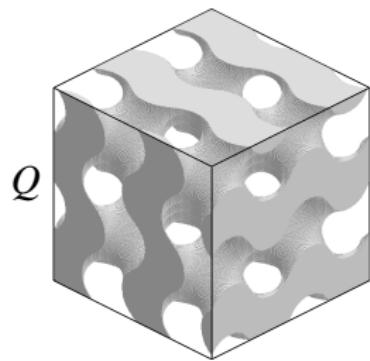
Test cases

ABC flow



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ABC flow



Test cases

Forced isotropic turbulence (Vincent & Meneguzzi, JFM, 1991)

- Q , λ_2 and H_ω regions: $\approx 40\%$ of the total volume
- conditional averaging of $\left\{ \begin{array}{l} k, \epsilon, \Omega^2/S^2 \\ \text{terms of the enstrophy equation} \end{array} \right.$
- differences between H_ω and (Q, λ_2) regions
 - higher ϵ (inverse trend)
 - enstrophy equation: $\left\{ \begin{array}{ll} \text{lower} & \text{dis}_{\omega^2} \\ \text{higher} & P_{\omega^2}, \text{dif}_{\omega^2}, D_{\omega^2} \end{array} \right.$
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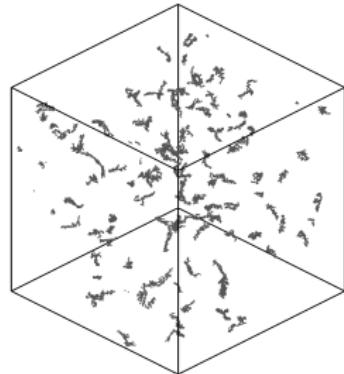
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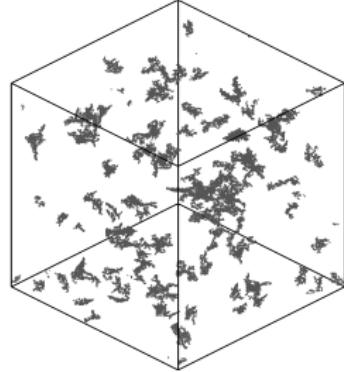
Freely decaying homogeneous turbulence (Liechtenstein, Godeferd & Cambon, JoT, 2005)

Isotropic

H_{ω}^p

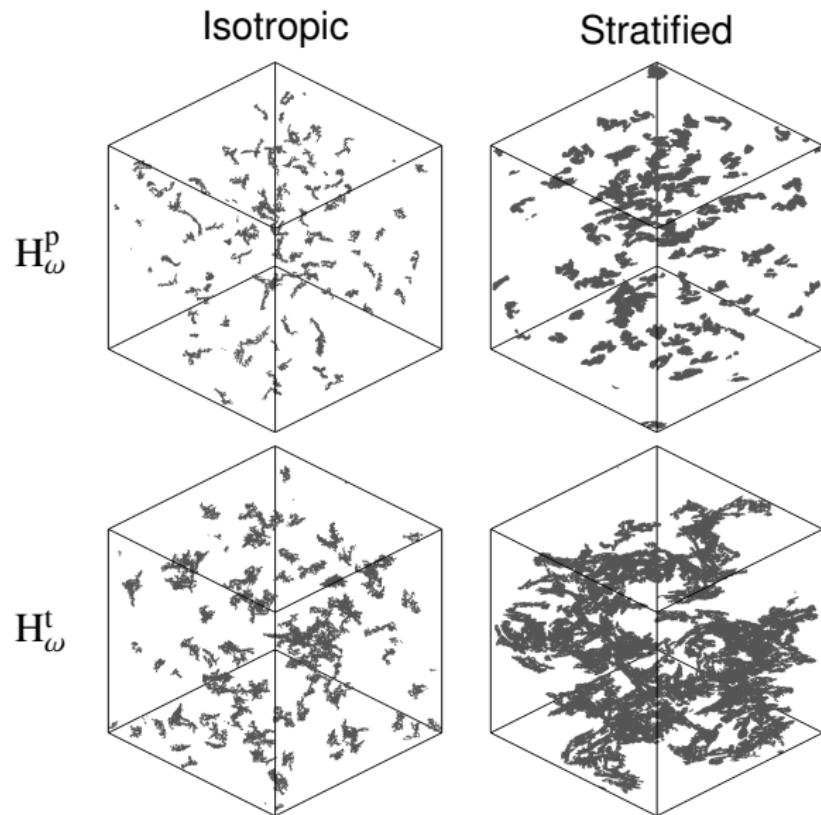


H_{ω}^t



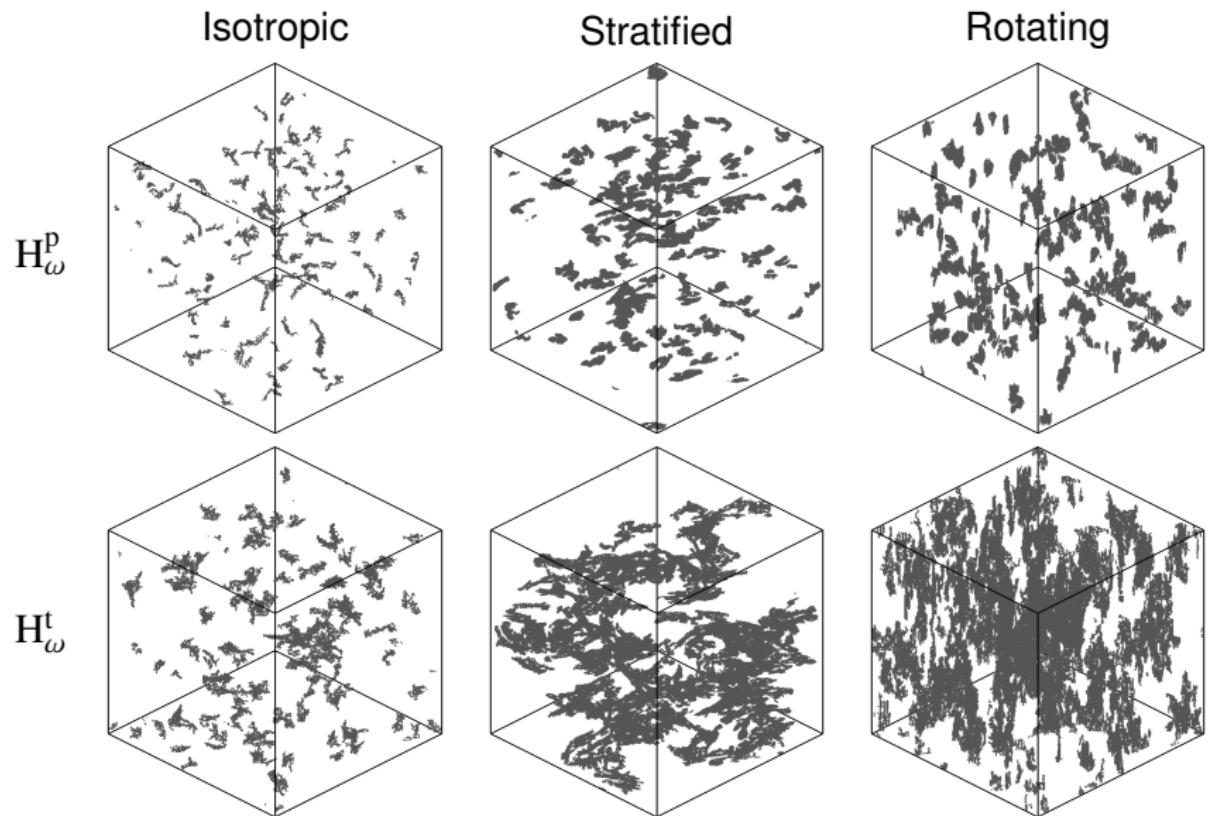
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Conclusion and future work

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- ... also related to maxima of ω
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- educe low percentages of the total volume ...
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- educe small scales structures ...
- ... with specific enstrophy dynamics: $\left\{ \begin{array}{l} \text{high vortex stretching} \\ \text{high diffusion} \\ \text{low dissipation} \end{array} \right\} \dots$
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Definitions of the members of the H_ω family

	H_ω^p	H_ω^t	$H_\omega^{rl\varrho}$	$H_\omega^{s\varrho}$	$H_\omega^{rl\mathcal{H}}$	$H_\omega^{s\mathcal{H}}$
I_1	< 0	< 0	< 0	< 0	< 0	< 0
I_2	> 0	> 0	≤ 0	≤ 0	≤ 0	≤ 0
I_3	< 0	≥ 0	≥ 0	≥ 0	≥ 0	≥ 0
Q			> 0	≤ 0		
\mathcal{H}					> 0	≤ 0

Enstrophy equation: terms

- evolution equation for the enstrophy

$$\begin{aligned}\frac{D \frac{1}{2} \omega_i \omega_i}{Dt} &= \underbrace{\omega_i \omega_j S_{ij}}_{P_{\omega^2}} + \underbrace{\nu \omega_i \frac{\partial^2 \omega_i}{\partial x_j \partial x_j}}_{D_{\omega^2}} \\ &= \underbrace{\omega_i \omega_j S_{ij}}_{P_{\omega^2}} - \underbrace{\nu \frac{\partial \omega_i}{\partial x_j} \frac{\partial \omega_i}{\partial x_j}}_{dis_{\omega^2}} + \underbrace{\nu \frac{\partial^2 \frac{1}{2} \omega_i \omega_i}{\partial x_j \partial x_j}}_{dif_{\omega^2}}\end{aligned}$$

- Vortex Stretching Rate

$$V.S.R. = \frac{\omega_i \omega_j S_{ij}}{\omega_k \omega_k}$$

Detailed analysis for isotropic turbulence

Global criteria

	H_ω	Δ	Q	λ_2
V	42–44%	62–70%	39–42%	39–43%
k	0.96–0.98	0.98–0.99	0.96–0.98	0.97–0.99
ϵ	1.09–1.18	0.83–0.89	0.75–0.82	0.72–0.81
ω^2	1.51–1.55	1.24–1.36	1.66–1.82	1.61–1.78
P_{ω^2}	1.66–1.72	1.14–1.18	1.42–1.49	1.27–1.34
dis_{ω^2}	0.82–0.85	0.99–1.01	1.0–1.01	1.02–1.05
D_{ω^2}	1.89–2.08	1.2–1.27	1.56–1.65	1.56–1.68
V. S. R.	1.25–1.28	0.72–0.73	0.74–0.79	0.63–0.75
$\langle \Omega^2 \rangle / \langle S^2 \rangle$	1.28–1.42	1.39–1.57	2.02–2.31	2.0–2.36

Detailed analysis for isotropic turbulence

Subdivisions of H_ω

	H_ω^p	H_ω^t	$H_\omega^{rl\mathcal{H}}$	$H_\omega^{s\mathcal{H}}$
V	6–7%	11–12%	20–21%	4–5%
k	0.95–1.0	0.96–0.99	0.95–0.98	0.95–0.98
ϵ	1.09–1.39	1.11–1.33	1.04–1.07	1.07–1.1
ω^2	2.17–2.23	1.88–1.93	1.21–1.23	1.10–1.12
P_{ω^2}	2.57–2.85	2.25–2.34	1.2–1.26	1.2
dis_{ω^2}	0.90–1.05	0.87–0.92	0.77–0.84	0.67–0.72
D_{ω^2}	3.14–3.71	2.5–2.9	1.33–1.4	1.02–1.11
V. S. R.	1.37–1.51	1.38–1.43	1.09–1.19	1.16–1.18
$\langle Q^2 \rangle / \langle S^2 \rangle$	1.56–2.06	1.41–1.72	1.14–1.18	1.02–1.04